

DETechnologies

Final Presentation



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Agenda

- Preliminary Matter
- Analytical Models Results
- Final Design
- Final Computer Aided Design
- Finite Element Analysis
- Computational Finite Difference
- Manufacturing Drawings
- Preliminary Thrust Stand

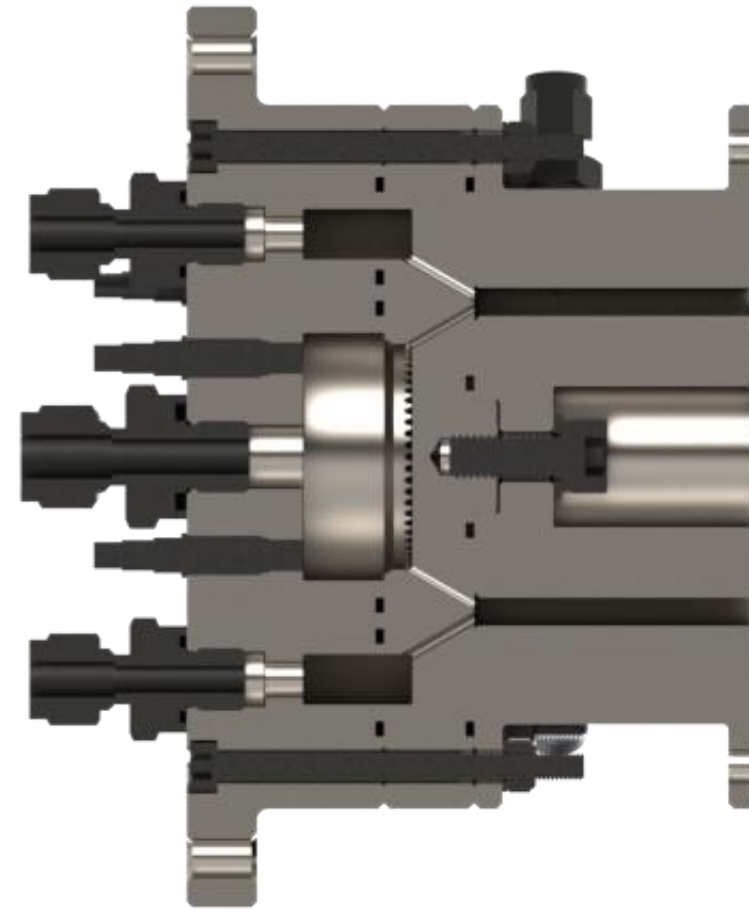


Figure: Cross-sectional view of the final prototype CAD assembly.

Preliminary Matter

Problem Definition: Very little literature is available that clearly outlines the design process involved in choosing engine sizing for any application.

Alternate RDE Design Approach: Trial and error engine sizing or borrow working experimental design.

Constraints:

- *Technical*
 - Lack of local technical expertise
 - Combustion temperature and pressure
- *Budgetary*
 - Propellant feed system estimated to be between \$50-100k [1]
 - Sensor prices estimated > \$20k
- *Safety*
 - No local combustion testing facility
 - GO₂ and GH₂ handling best practices [2][3][4].
- *Time*
 - Only 3 months from term start to finish

Budget:

Table: Table of accrued and estimated expenditures.

Description	Cost
ClickUp; Project Management Software	\$ 300.00
Metal Pros - Stock Metal	\$ 1,495.00*
Outsourced Machining Services	\$ 3,450.00*
Team Clothing	\$ 500.00
Total	\$ 5,745.00

Analytical Model(s) Final Form

Combustion Parameters

- Iterate over range of input parameters; minimize chamber Pressure & Temperature.

Injector Sizing

1. Iterate A_i/A_A ratio to reach desired plenum pressure.
2. Apply DFMA constraints, update plenum pressure.

Performance Prediction

1. Calculate geometry based on iterative I/P parameters.
2. Minimum h^* predicts low thrust (322N), increase mass flow rate to reach thrust target.

Equation: Mass Flow; Choking Condition; Rearranged for plenum stagnation pressure [5]

$$P_o = \dot{m}A \sqrt{\frac{\gamma}{RT_o}} \left(1 + \frac{\gamma - 1}{2}\right)^{-\frac{\gamma+1}{2(\gamma-1)}}$$

Equation: Mass Flow; Total Required [6]

$$\dot{M} = HW \rho_c U_{cJ}$$

Equation: Specific Thrust; Rearrange \dot{M} to get T [6]

$$\left. \frac{T}{\dot{M}} \right|_{P_a} = \sqrt{2C_p T_1} \left[1 + \frac{q}{C_p T_1} - \left(\frac{P_a}{P_1} \right)^{(\gamma-1)/\gamma} \left(\frac{P_1}{P_2} \right)^{(\gamma-1)/\gamma} \frac{T_2}{T_1} \right]^{1/2}$$

Equation: Detonation Cell Size [10]

$$\lambda = \lambda_{ref} \frac{P_{ref}}{P}$$

Equation: Minimum Fill Height Correlation [7] [8]

$$l_{f,cr} = (12 \pm 5)\lambda$$

Analytical Model(s) Final Form

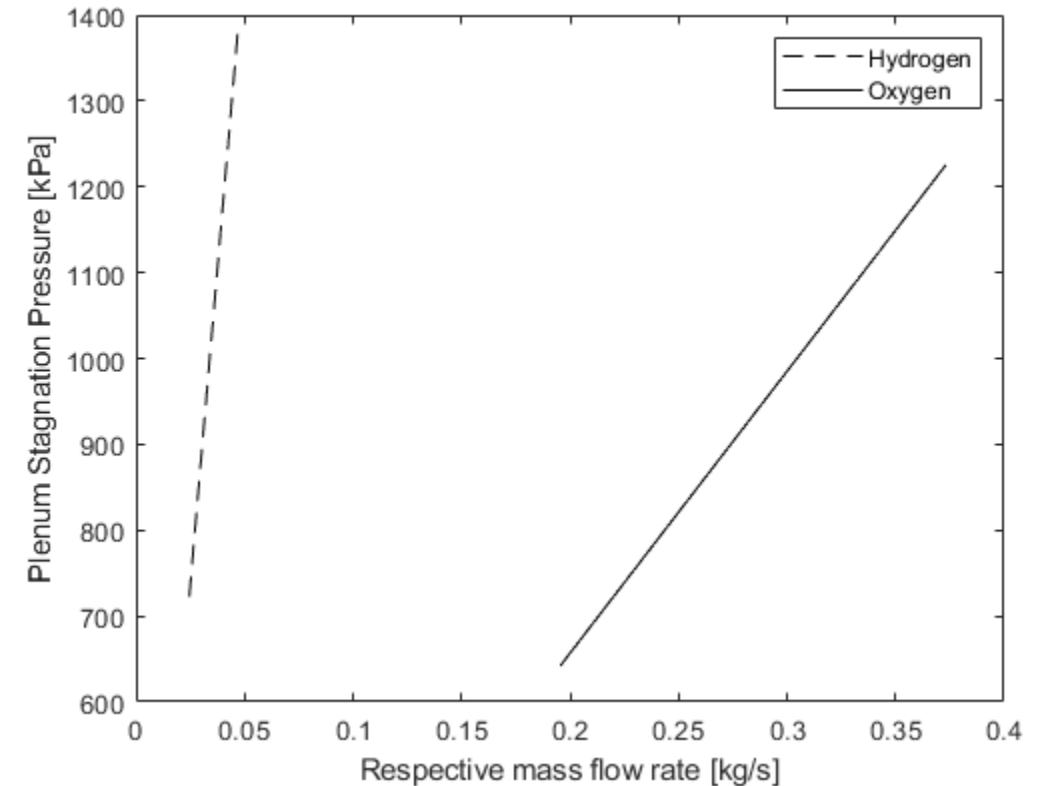
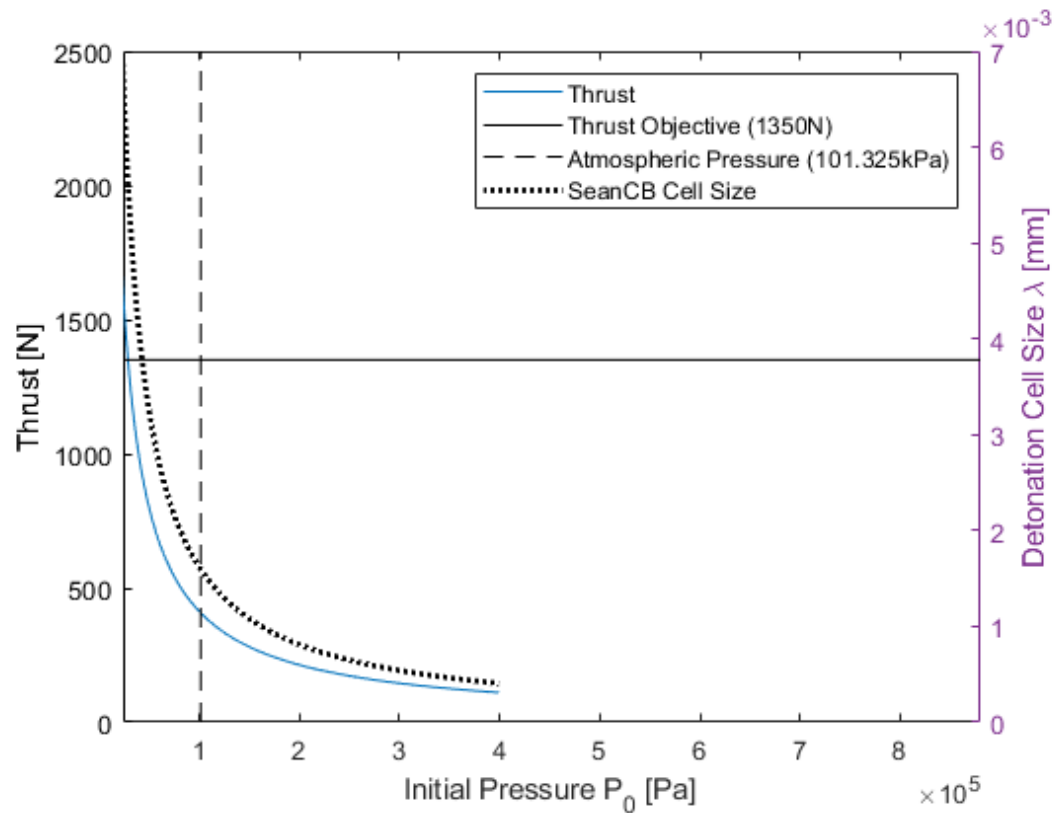


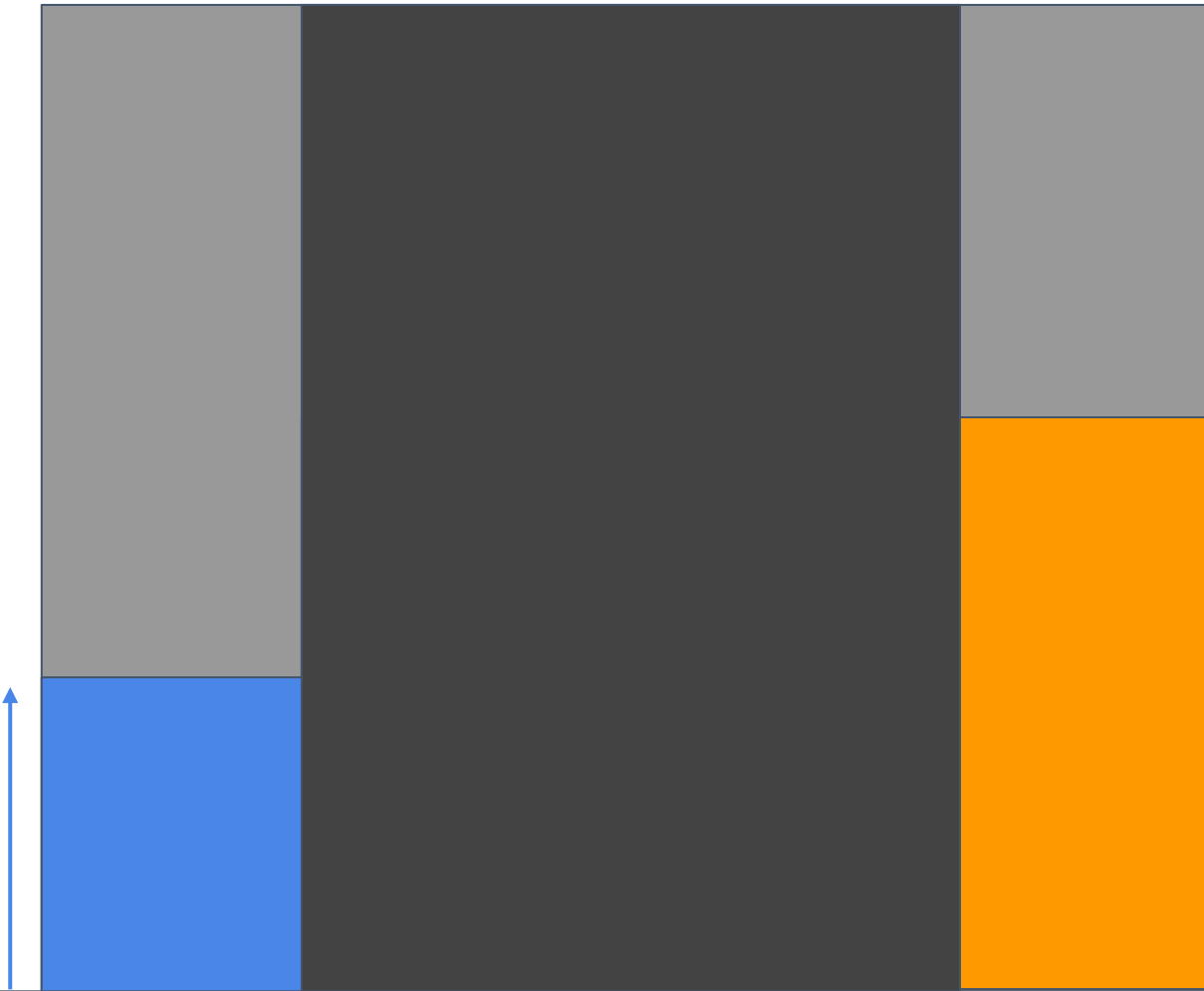
Figure: Thrust for initial chamber pressures and detonation cell sizes; with 1 atm and target thrust indicated.

Figure: Mass flow rate and plenum pressures for fuel and oxidizer.

Analytical Model(s) Final Form

Minimum propellant volume to achieve detonation.

h^*_{min}



Propellant volume to reach thrust target.

$h^*_{desired}$

Final Design Parameters

Table: Summary of Combustion Parameters

Parameter	Value
Detonation Cell Size, λ	1.214707 mm
Initial Temperature, T_0	300 K
Initial Pressure, P_0	130 kPa
Equivalence Ratio, ϕ	1.00
Mass Flow Rate, \dot{m}	3.20 $\frac{kg}{s}$
Specific Impulse, I_{SP}	410.6716 s
Peak Pressure, P_{VN}	4299196.4247 Pa
Peak Temperature, T_{CJ}	3720.2403 K
Combustion Speed, V_{CJ}	2848.5565 $\frac{m}{s}$

Table: Summary of Engine Geometry

Parameter	Value
Detonation Cell Size, λ	1.214707 mm
Thrust Goal	1350 N
Fill Height, h^*	$h^* > 14.964923$ mm
Chamber Outer Diameter, D	60.00 mm
Chamber Inner Diameter, D	50.00 mm
Channel Width, δ	5.00 mm
Length, L	50.00 mm

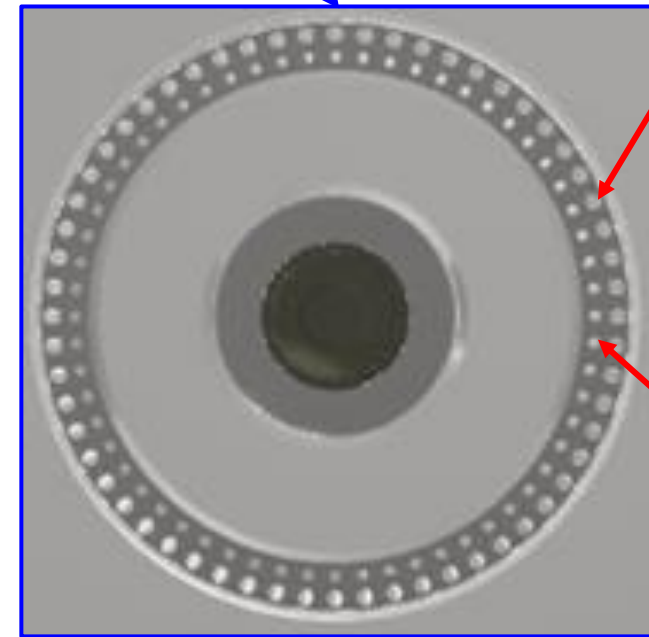
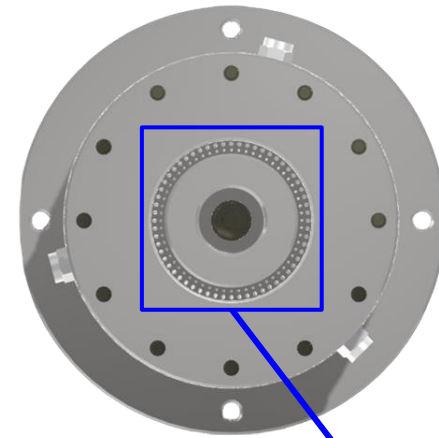
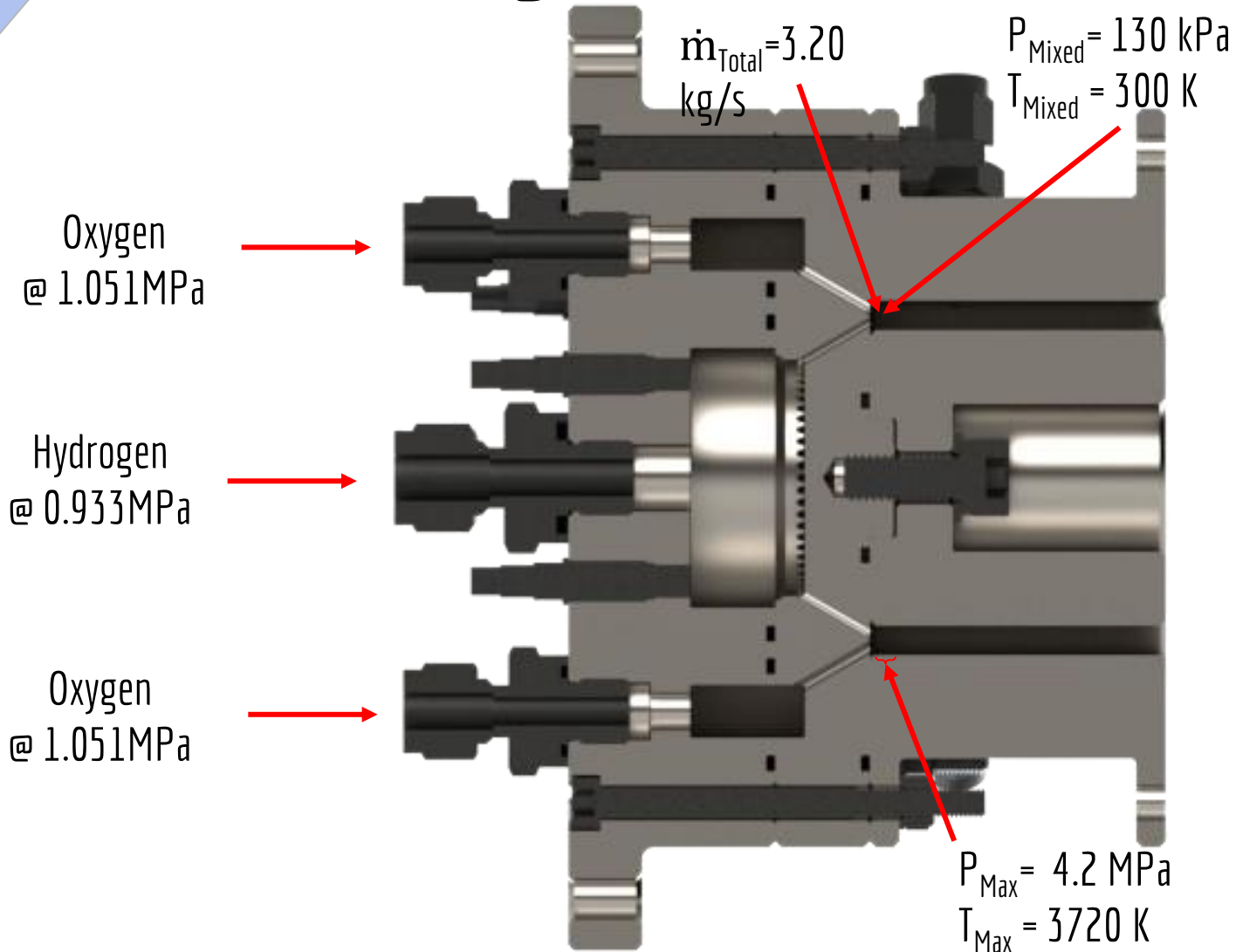
Table: Summary of Injector Plate Parameters

Parameter	Value
Hydrogen Plenum Pressure, P_h	1051.096564 kPa
Hydrogen Injector Area Ratio, A_h	5.4545 %
Hydrogen Injector Specifics	60 x ϕ 1 mm
Oxygen Plenum Pressure, P_O	933.436855 kPa
Oxygen Injector Area Ratio, A_O	12.2727 %
Oxygen Injector Specifics	60 x ϕ 1.5 mm

Table: Summary of Validation Paper Parameters [10]

Parameter	Proposed Engine	American Engine
Thrust Target [N]	1350	1350
Designed Specific Impulse [s]	414	-
Mass Flow Rate [g/s]	320	270-375
Outer Diameter [mm]	60	76.2 (3")
Inner Diameter [mm]	50	66.2
Equivalence Ratio, ϕ	1.0	1.1-1.7
Number of Waves	2	2-3

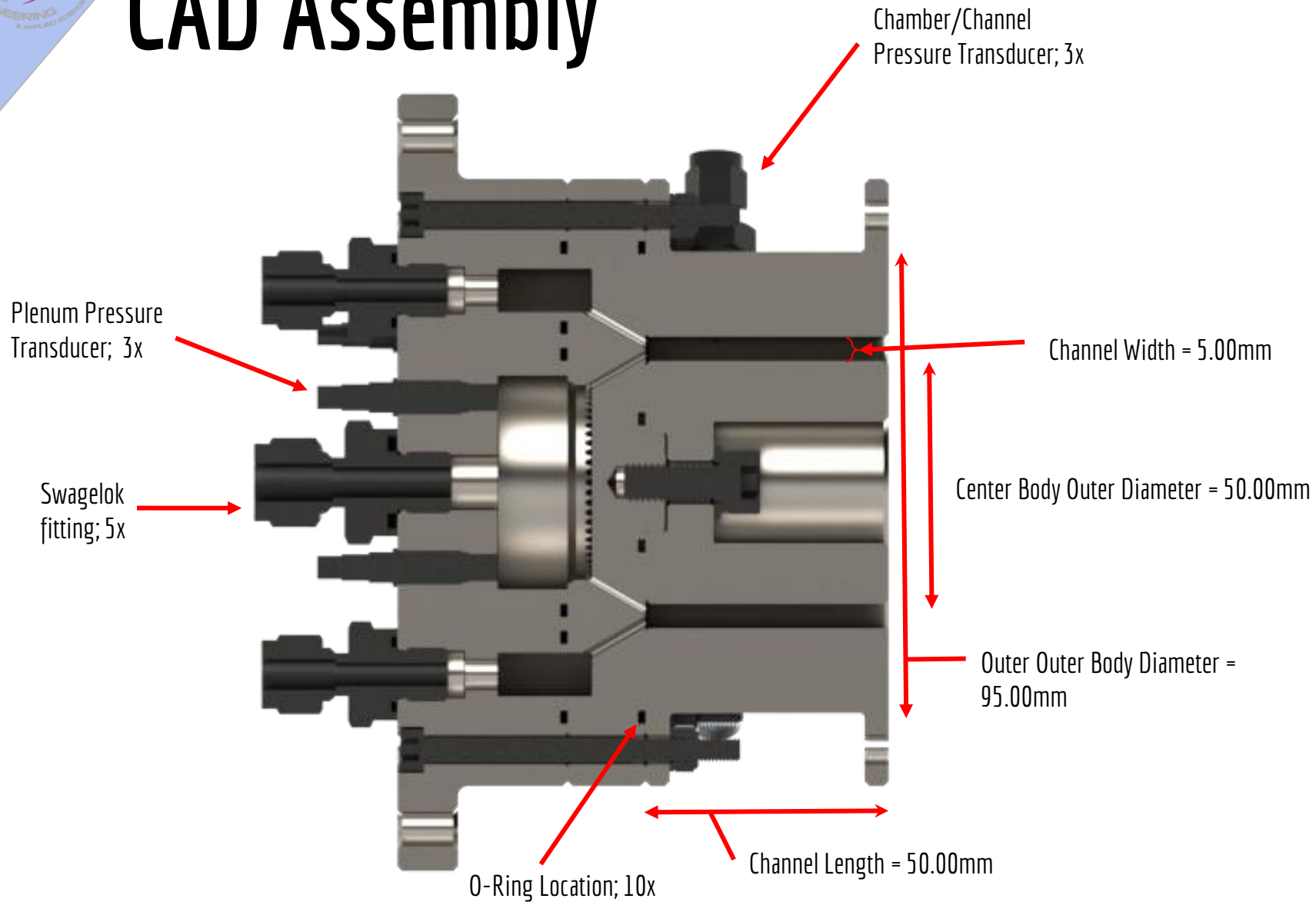
Final Design Parameters



60 x 1.50mm O₂

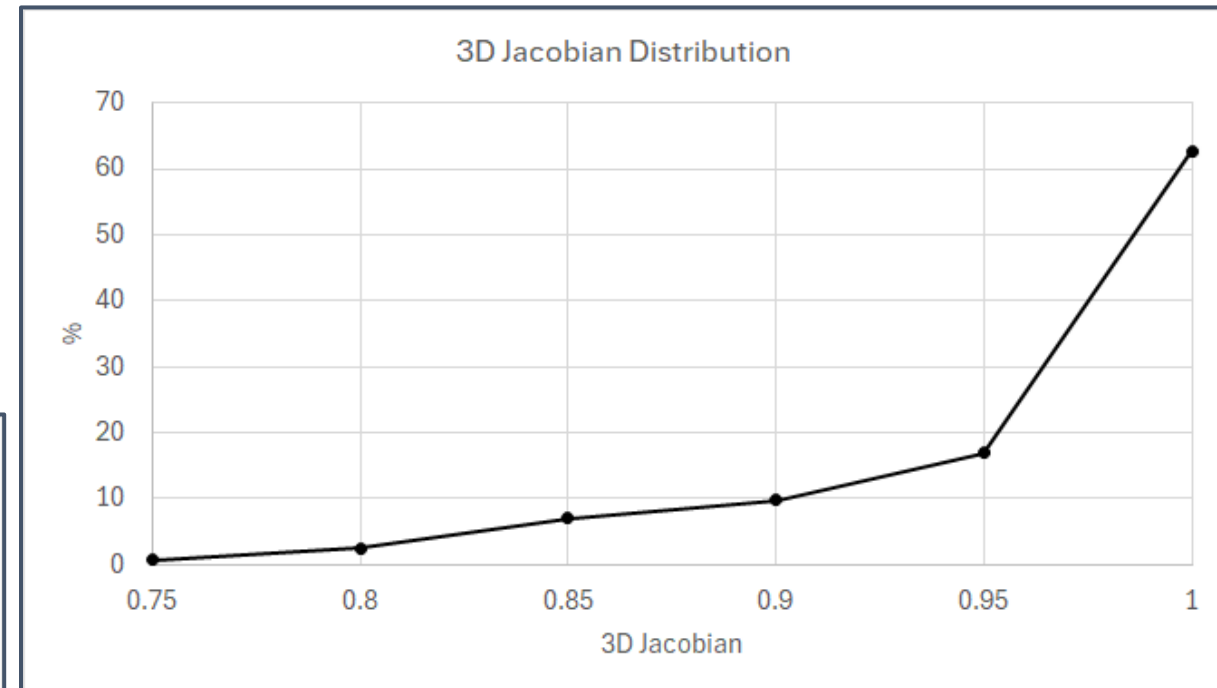
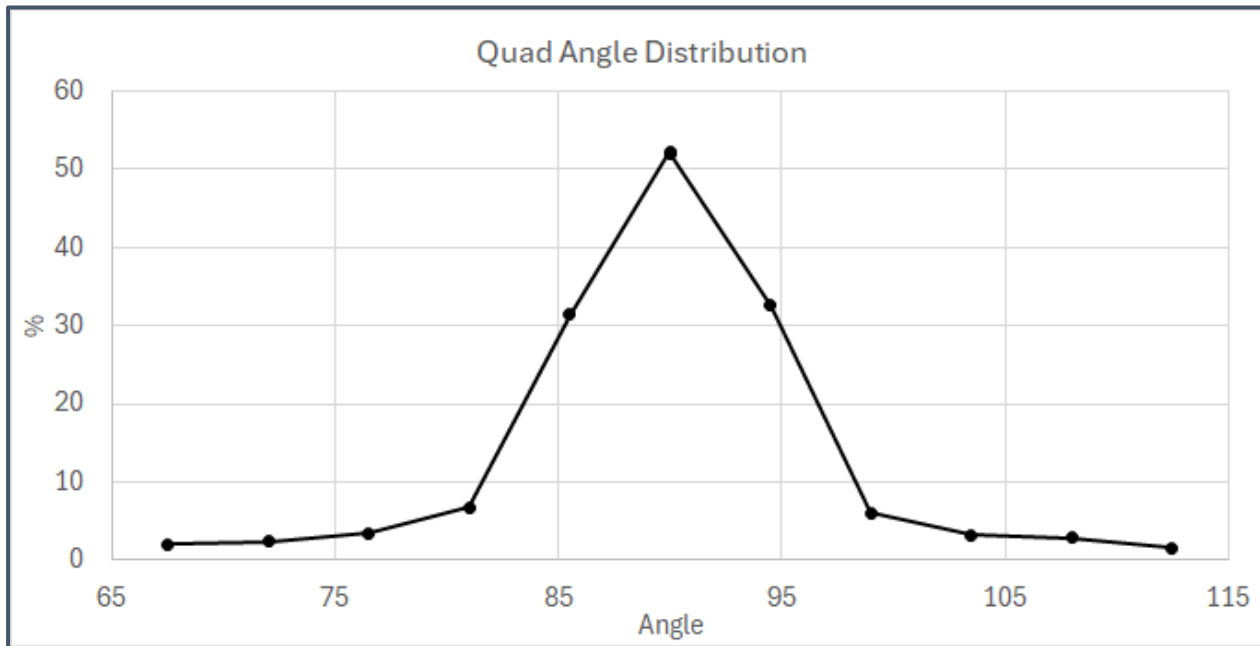
60 x 1.00mm H₂

CAD Assembly



FEA: Model Setup & Mesh

Element Type	Percentage of Mesh
Hexahedral (1st Order)	97.43 %
Pentahedral (1st Order)	2.57 %



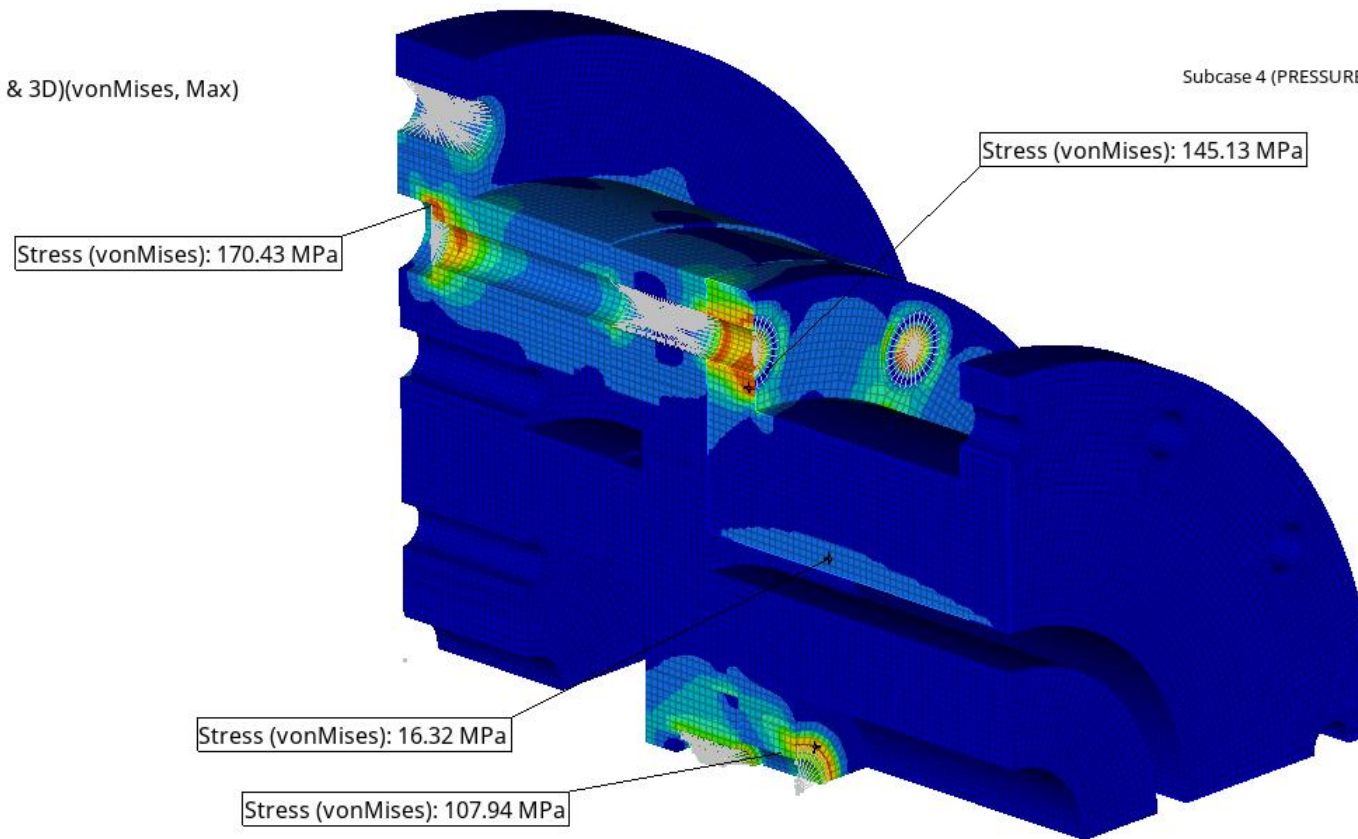
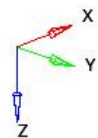
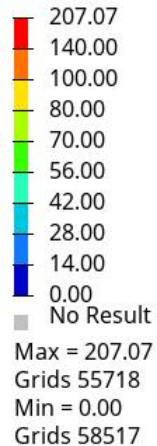
- Linear isotropic material card, using material properties for AISI 316 Stainless Steel from Washko et al., ASM [11]
- 1-D bolted joint modelling using BEAM's and RBE's

FEA: Static Loading (Pressure)

Pressure applied to inner walls of combustion chamber, center body and exposed surface of injector plate

- Pressure (as per VN Spike): 4.3 MPa

Contour Plot
Element Stresses (2D & 3D)(vonMises, Max)
Analysis system
Simple Average

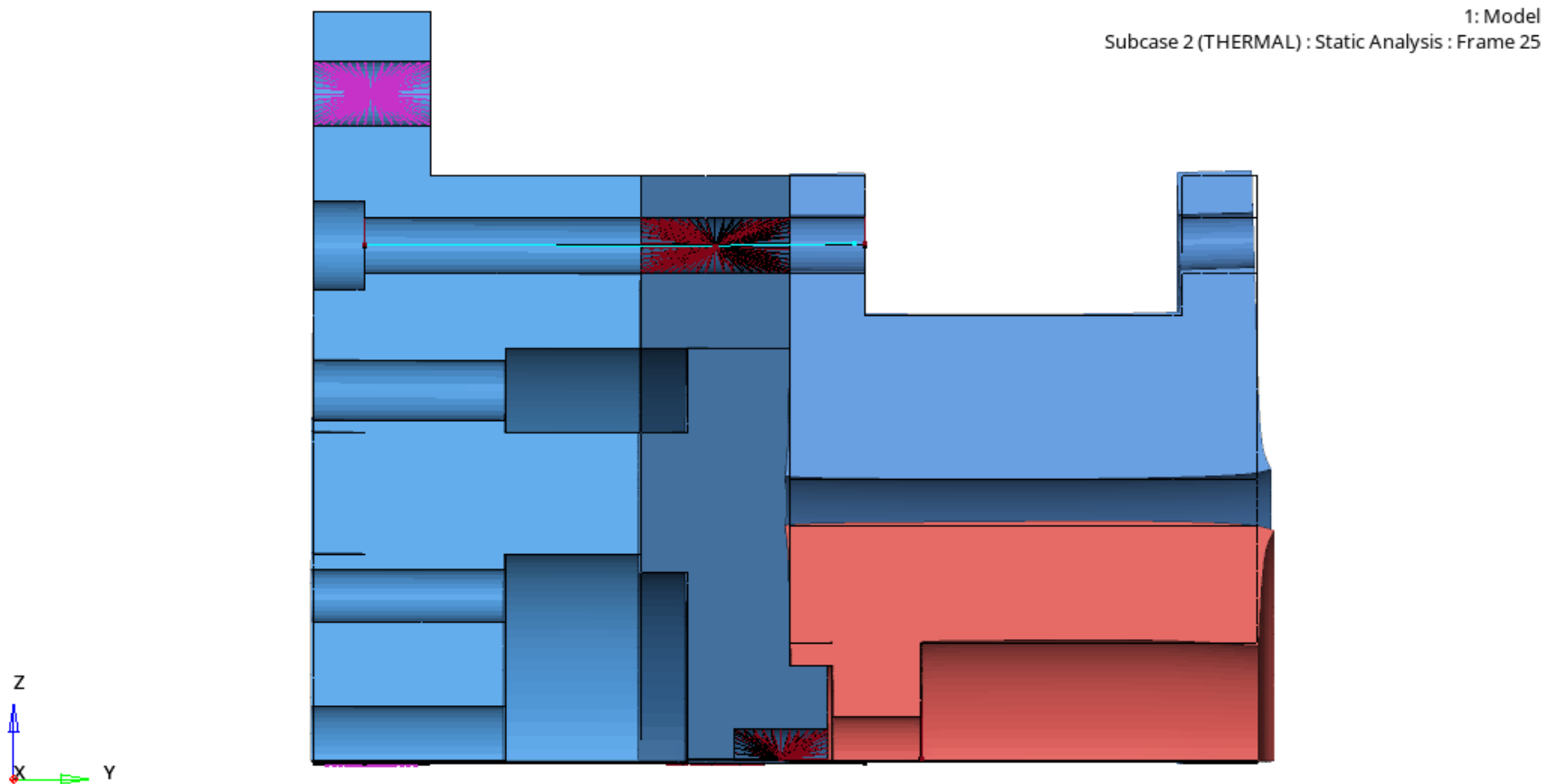


1: Model
Subcase 4 (PRESSURE) : Static Analysis : Frame 25

FEA: Static Loading (Temperature)

Temperature applied to inner walls of combustion chamber, center body and exposed surface of injector plate

- Temperature as per analytical model: 3500 K

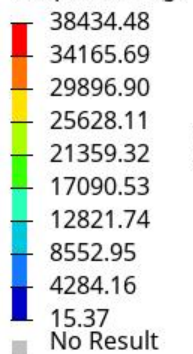


FEA: Static Loading (Temperature)

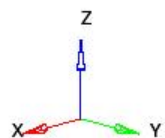
Temperature applied to inner walls of combustion chamber, center body and exposed surface of injector plate

- Temperature as per analytical model: 3500 K

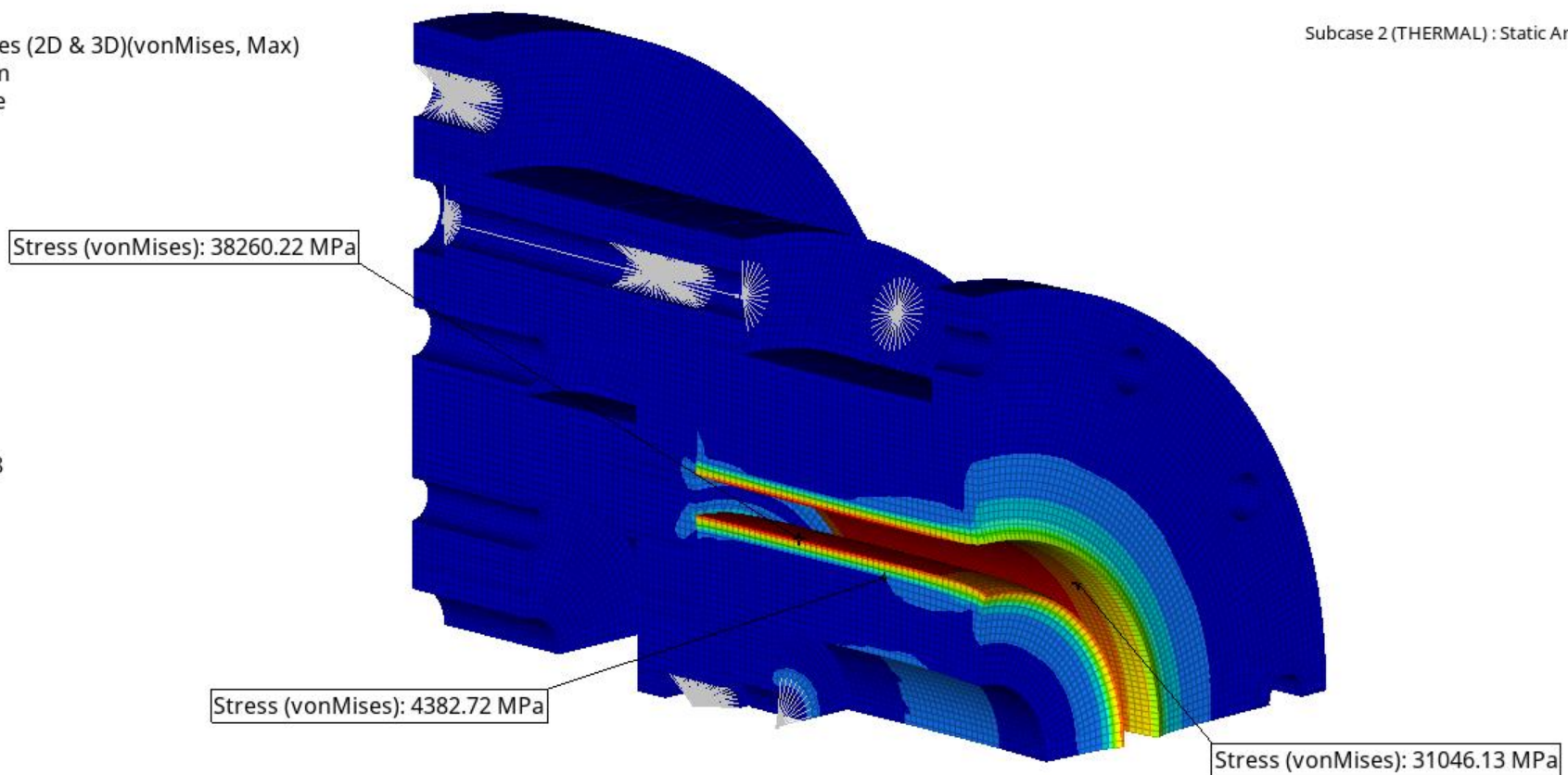
Contour Plot
Element Stresses (2D & 3D)(vonMises, Max)
Analysis system
Simple Average



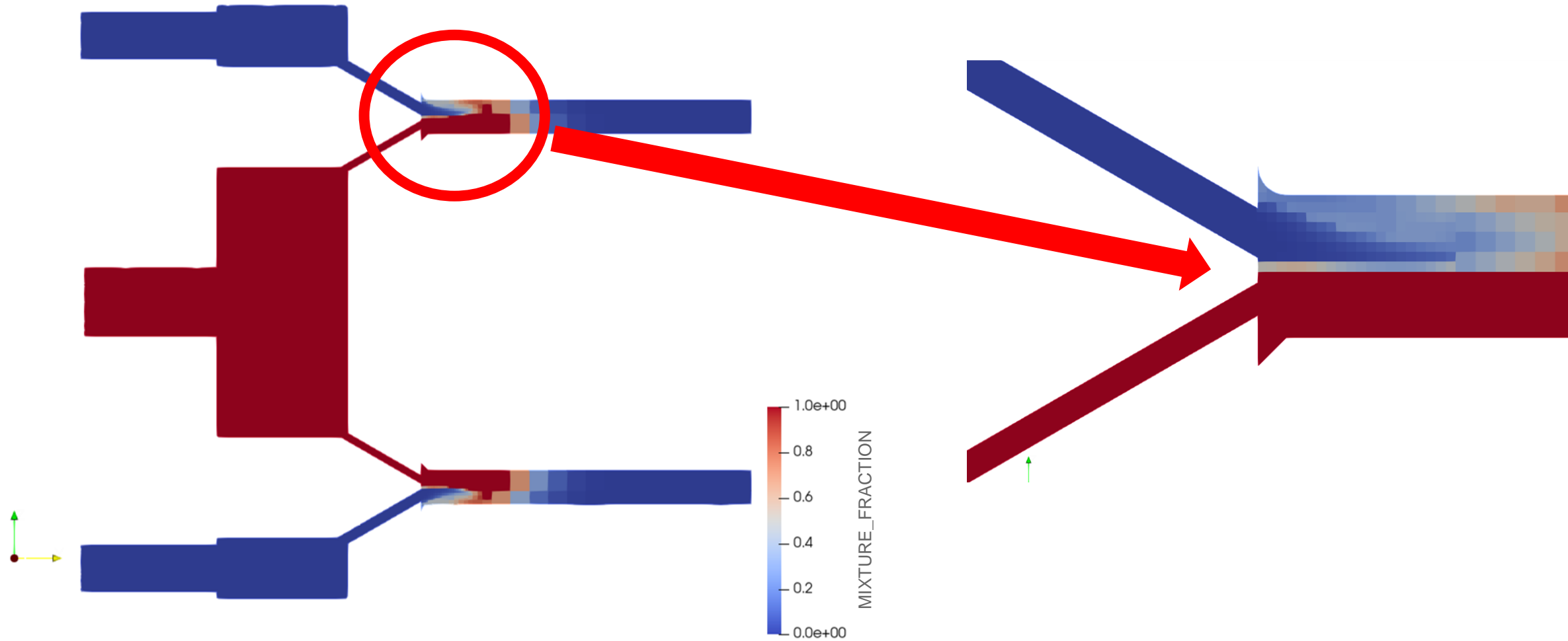
Max = 38434.48
Grids 632004
Min = 15.37
Grids 877591



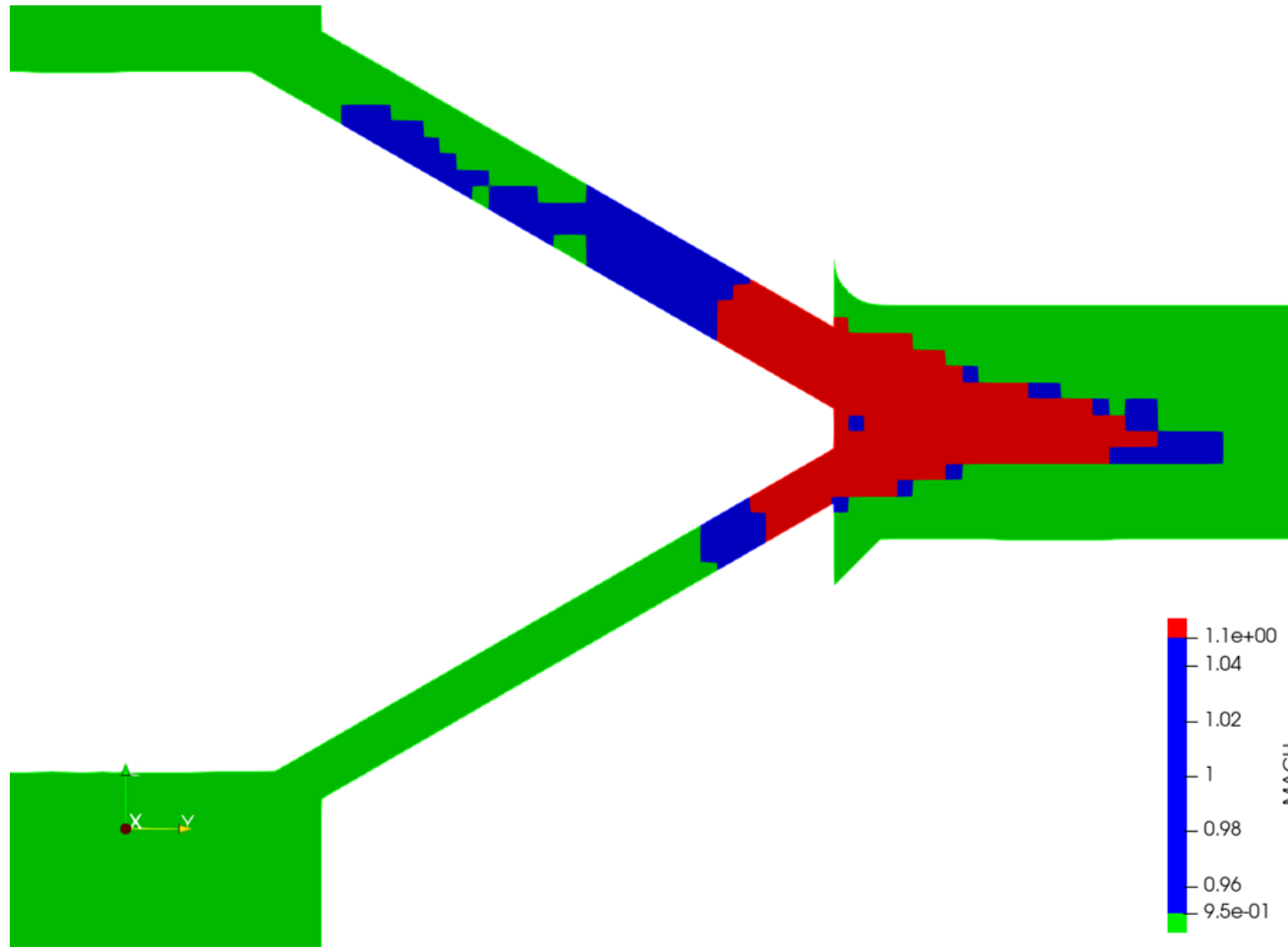
1: Model
Subcase 2 (THERMAL) : Static Analysis : Frame 25



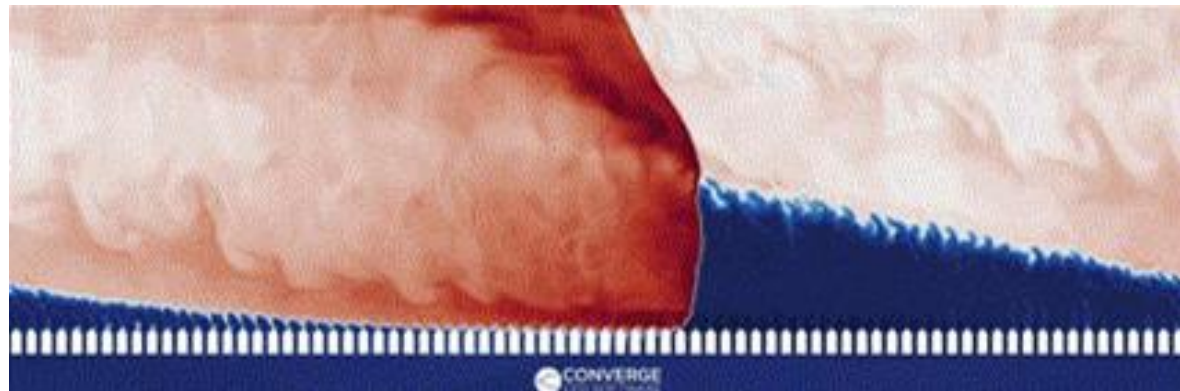
CFD: Injector Flow



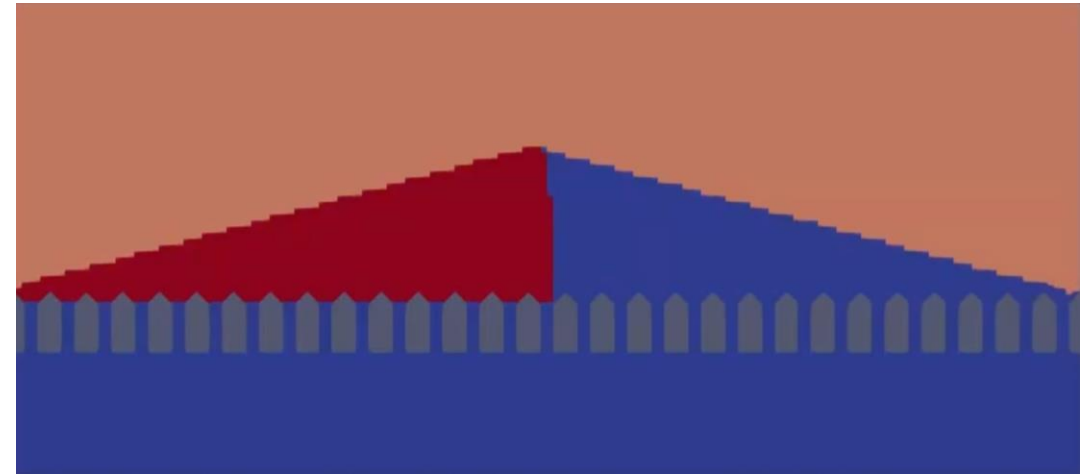
CFD: Injector Flow



CFD: Combustion



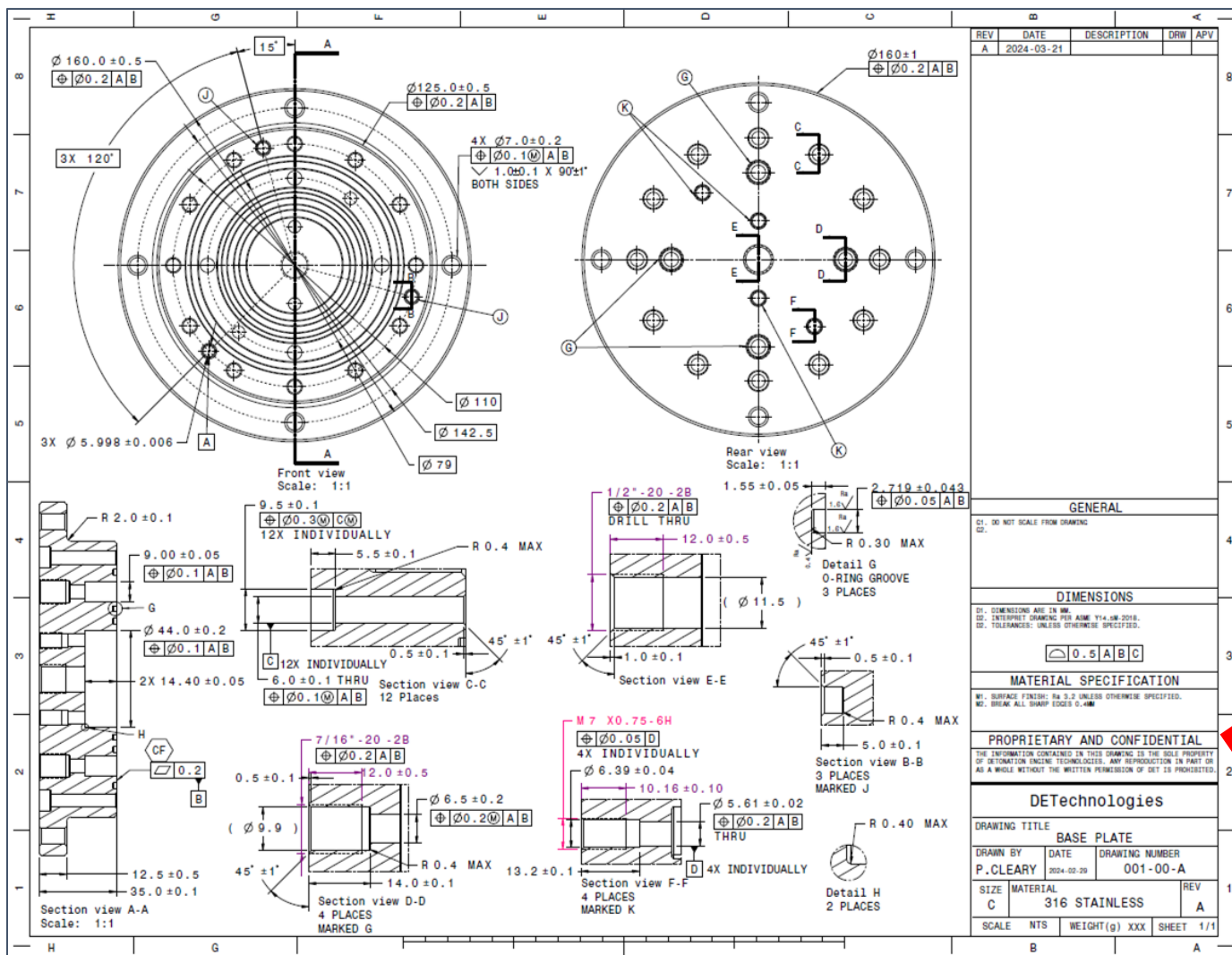
Video: 2D RDE Simulation using ConvergeCFD, by Convergent Science [12]



Video: Our 2D RDE - Best Progress yet

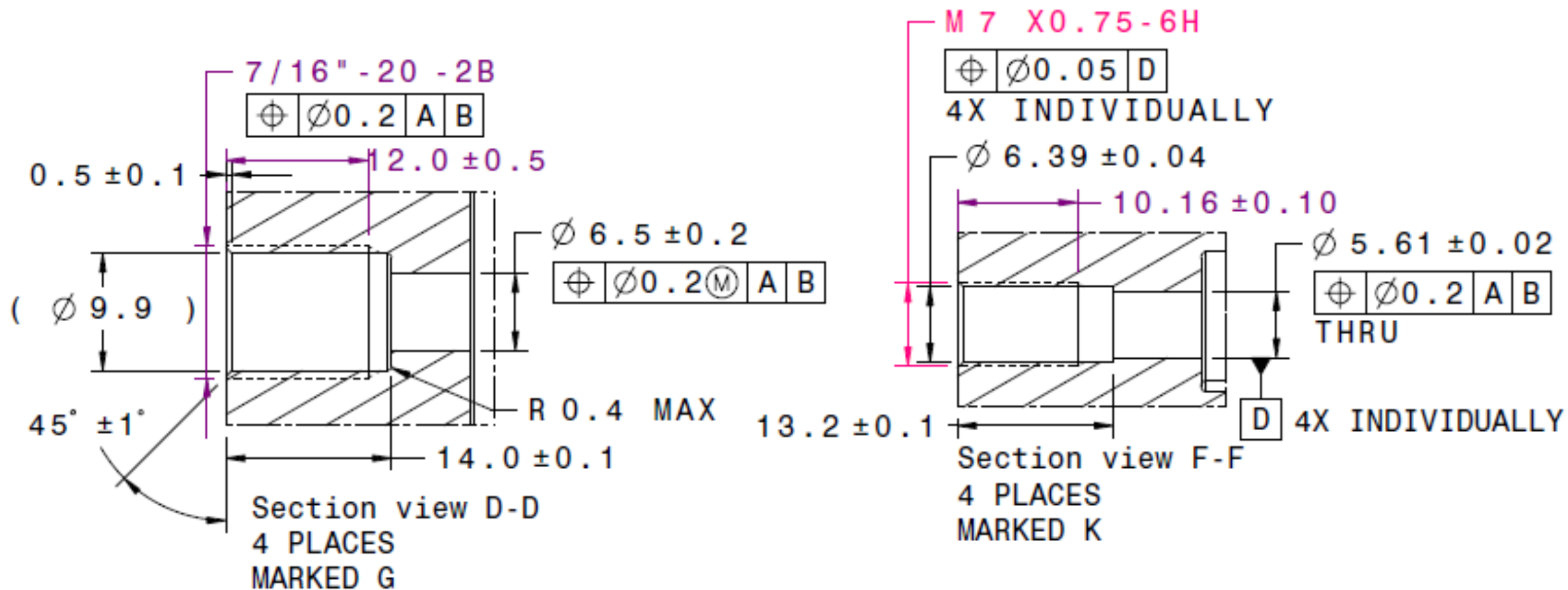


DFMA & Manufacturing Drawings

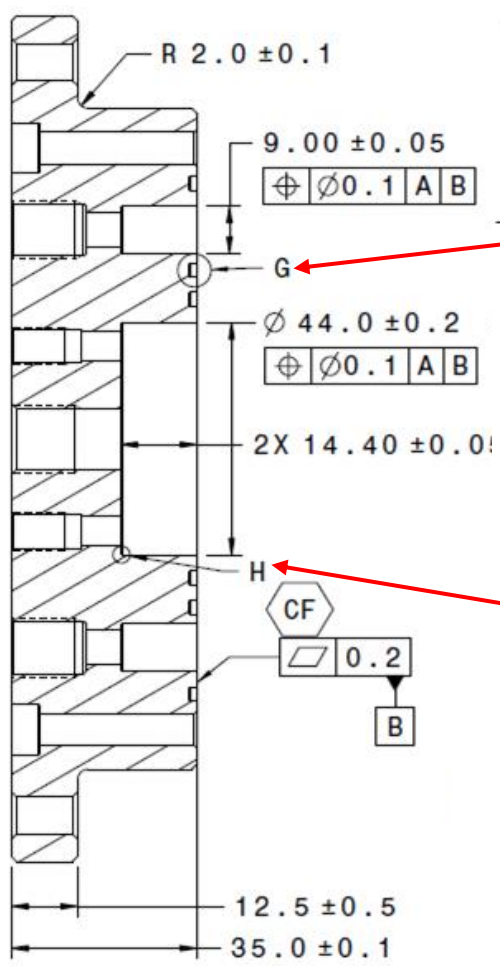


GENERAL		
G1. DO NOT SCALE FROM DRAWING G2.		
DIMENSIONS		
D1. DIMENSIONS ARE IN MM. D2. INTERPRET DRAWING PER ASME Y14.5M-2018. D2. TOLERANCES: UNLESS OTHERWISE SPECIFIED.		
MATERIAL SPECIFICATION		
M1. SURFACE FINISH: Ra 3.2 UNLESS OTHERWISE SPECIFIED. M2. BREAK ALL SHARP EDGES 0.4MM		
PROPRIETARY AND CONFIDENTIAL		
THE INFORMATION CONTAINED IN THIS DRAWING IS THE SOLE PROPERTY OF DETONATION ENGINE TECHNOLOGIES. ANY REPRODUCTION IN PART OR AS A WHOLE WITHOUT THE WRITTEN PERMISSION OF DET IS PROHIBITED.		
DETechnologies		
DRAWING TITLE		
BASE PLATE		
DRAWN BY	DATE	DRAWING NUMBER
P. CLEARY	2024-02-29	001-00-A
SIZE	MATERIAL	REV
C	316 STAINLESS	A
SCALE	NTS	WEIGHT(g) XXX SHEET 1/1

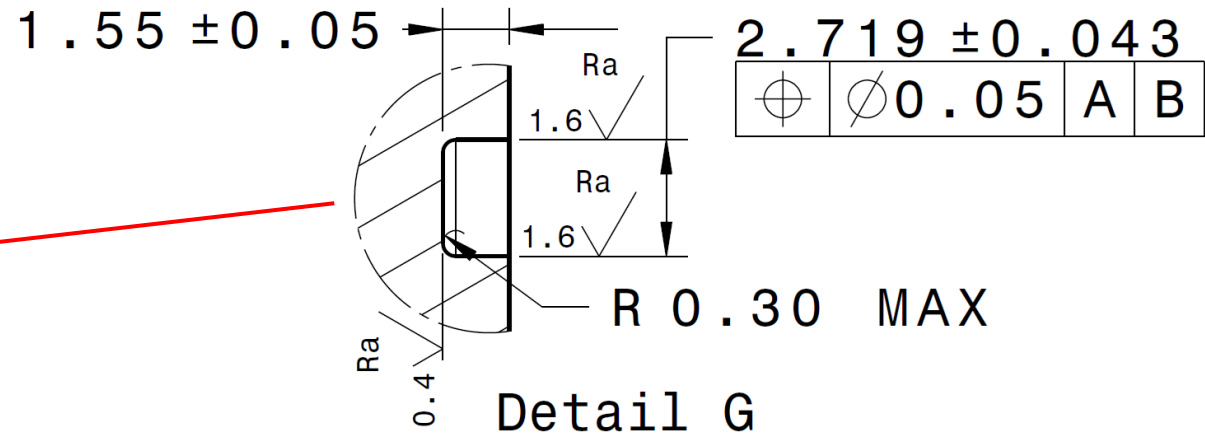
DFMA & Manufacturing Drawings



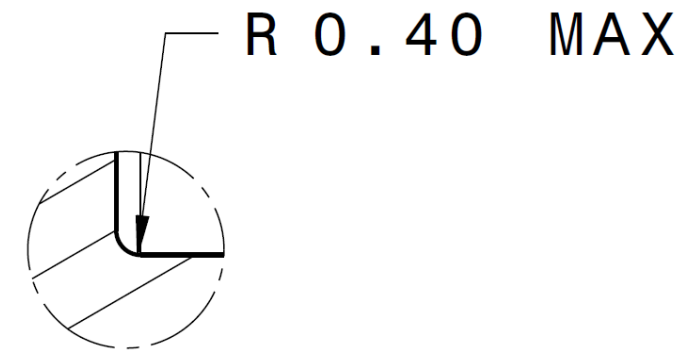
DFMA & Manufacturing Drawings



Section view A-A
Scale: 1:1



Detail G
O-RING GROOVE
3 PLACES



Detail H
2 PLACES

Multi-Axis Thrust Stand Design

Objective: Measure multi-axis thrust generation.

- Inherent vibrational instability / thrust vectoring effect due to rotating wave.

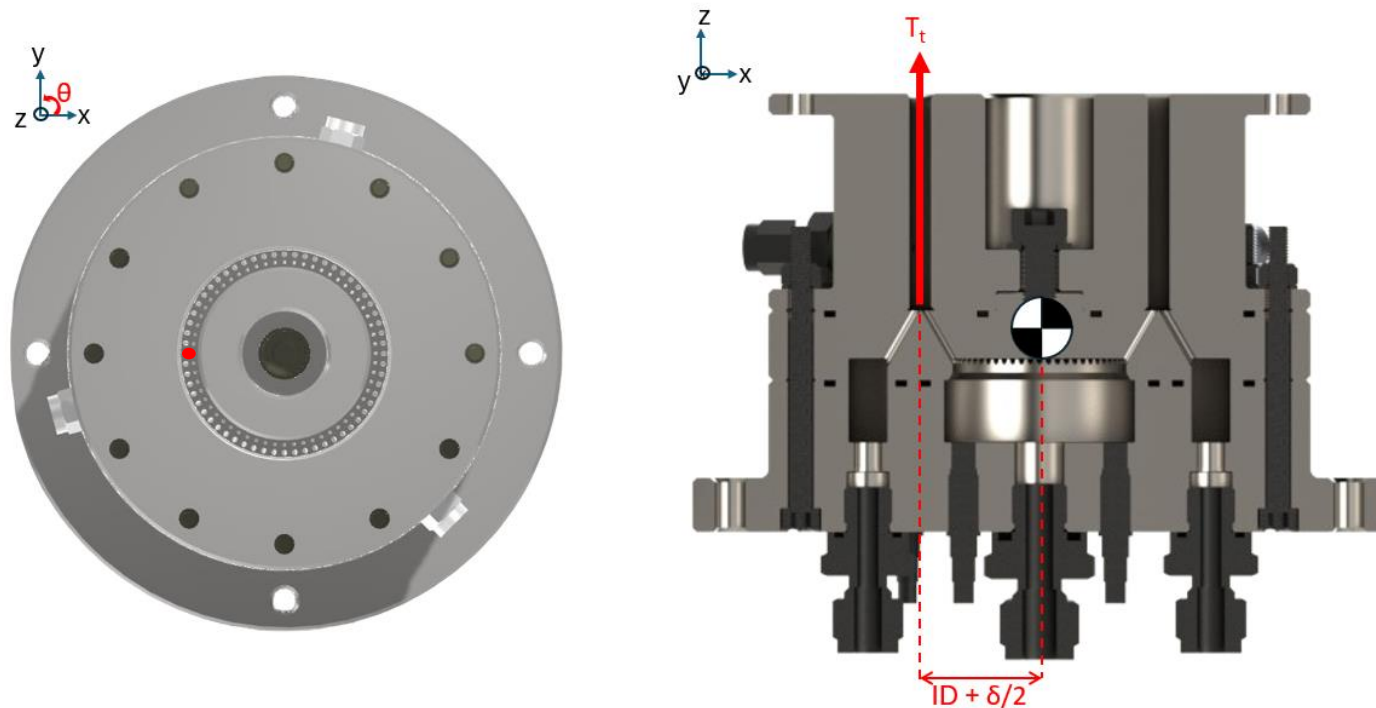


Figure: Schematics of Thrust Vectoring Moment

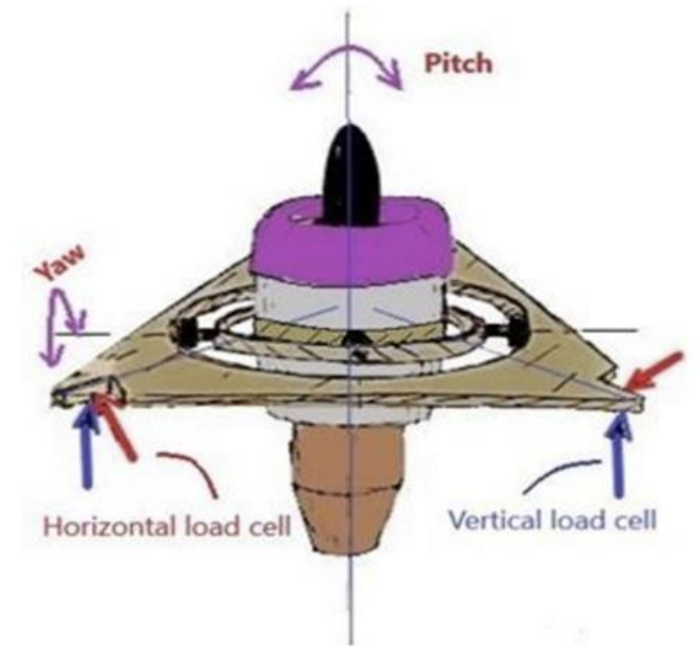


Figure: Schematic Showing Conceptual Thrust Stand DOF [13]

Multi-Axis Thrust Stand Design

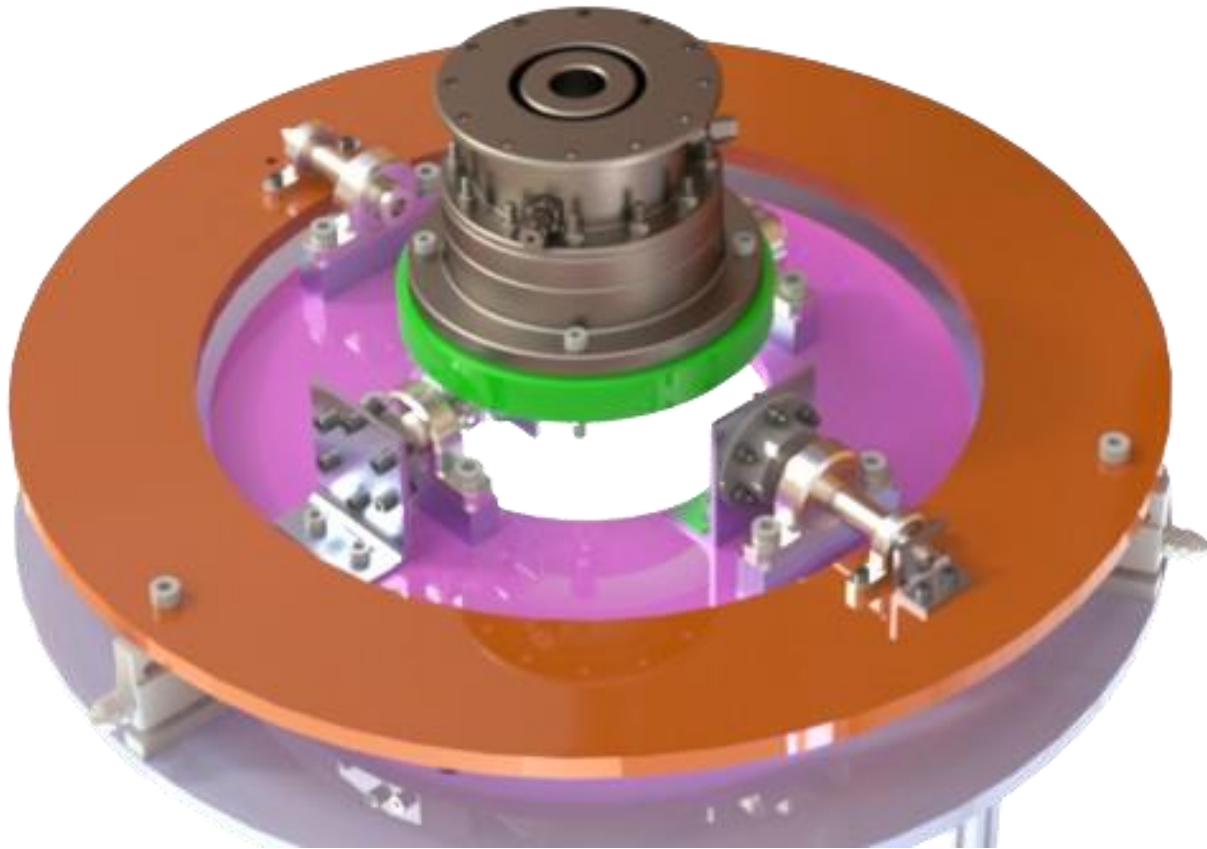


Figure: Preliminary Thrust Stand Design



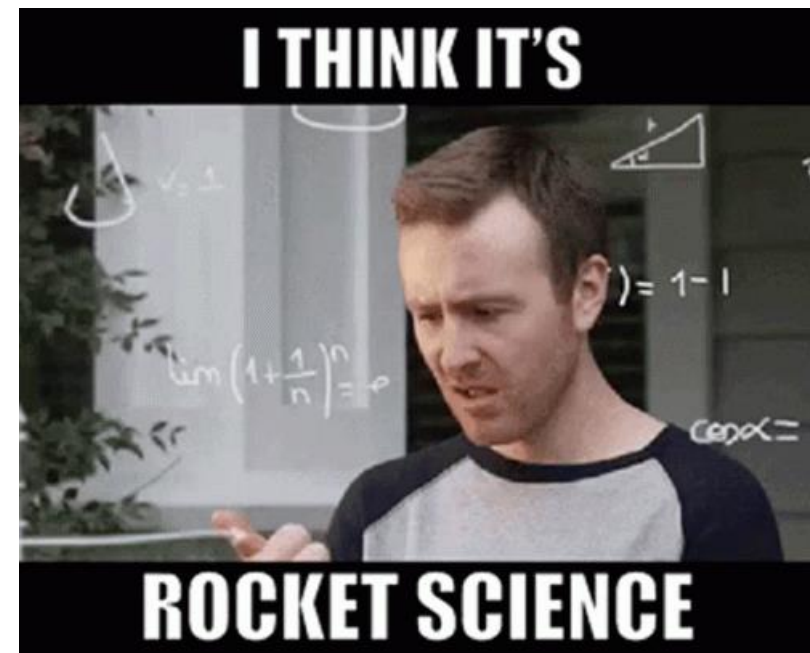
Video: Showing Degrees of Freedom

- [1] A. Higgins and C. Kiyanda, private communication, Jan 2024.
- [2] M. Lightfoot, S. A. Danczyk, J. Watts, and S. Schumaker, “Accuracy and best practices for small-scale rocket engine testing,” in JANNAF 2011 Joint Subcommittee Meeting, 2011.
- [3] P. M. Ordin, “Safety standard for hydrogen and hydrogen systems guidelines for hydrogen system design, materials selection, operations, storage and transportation,” 1997.
- [4] P. M. Ordin et al., “Safety standard for oxygen and oxygen systems-guidelines for oxygen system design, materials selection, operations, storage, and transportation,” NASA NSS, vol. 1740, 1996.
- [5] N. Hall, “Mass flow choking,” Mass Flow Choking, <https://www.grc.nasa.gov/www/k-12/airplane/mf1chk.html> (accessed Mar. 24, 2024).
- [6] J. E. Shepherd and J. Kasahara, “Analytical models for the thrust of a rotating detonation engine,” 2017.
- [7] F. A. Bykovskii, S. A. Zhdan, and E. F. Vedernikov, “Continuous spin detonations,” *Journal of propulsion and power*, vol. 22, no. 6, pp. 1204–1216, 2006.
- [8] A. P. Nair, A. R. Keller, N. O. Minesi, D. I. Pineda, and R. M. Spearrin, “Detonation cell size of liquid hypergolic propellants: Estimation from a non-premixed combustor,” *Proceedings of the Combustion Institute*, vol. 39, no. 3, pp. 2757–2765, 2023.
- [9] S. F. Connolly-Boutin, *Detonation Physics-Based Modelling & Design of a Rotating Detonation Engine*. PhD thesis, Concordia University, 2019.
- [10] J. W. Bennewitz, J. R. Burr, B. R. Bigler, R. F. Burke, A. Lemcherfi, T. Mundt, T. Rezzag, E. W. Plaehn, J. Sosa, I. V. Walters, et al., “Experimental validation of rotating detonation for rocket propulsion,” *Scientific Reports*, vol. 13, no. 1, p. 14204, 2023.
- [11] S. Washko and G. Aggen, “Wrought Stainless Steels,” in *Properties and Selection: Irons, Steels, and High-Performance Alloys*, ASM International, 01 1990.
- [12] “Simulating supersonic combustion in an unwrapped rotating detonation engine,” *Convergent Science*, <https://www.youtube.com/watch?v=7Q2d9vIWdNQ> (accessed Feb. 12, 2024).
- [13] R. N. Rezende, L. R. Alves, A. Mishra, H. Shukla, H. Varshney, H. Dhawan, S. Kapoor, U. Jain, and R. Mendonsa, “Designing a thrust vector test stand for the turborocket,” in *AIAA Propulsion and Energy 2021 Forum*, p. 3350, 2021.



<https://www.pinterest.ca/pin/4925880820403094/>

Thank-you



<https://tenor.com/view/rocket-science-complicated-difficult-challenging-math-gif-23793443>